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Nitrogen Dioxide Absorption Coefficients at High Temperatures

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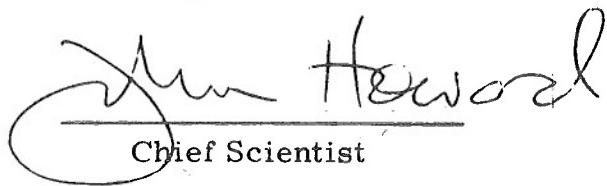
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This technical report has been reviewed and
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FOR THE COMMANDER



John Howard
Chief Scientist

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) The absorption coefficient of nitrogen dioxide, NO ₂ , is used in models of the fireball resulting from atmospheric nuclear detonations. This report gives values for the absorption coefficient obtained at wavelengths between 380 and 760 nm and at temperatures between 669 and 1313°K. The absorption coefficient varies from a maximum of about 10 cm ⁻¹ near 400 nm to about 0.1 cm ⁻¹ at the longest wavelength observed. The results agree with previously published data, which were available for only a few wavelengths, and provide a		

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comprehensive data set over the temperature and wavelength regions studied. Comparison of these results is made with NO₂ thermal emission intensities.

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Nitrogen Dioxide Absorption Coefficients at High Temperatures

I. INTRODUCTION

In 1970, Paulsen, Sheridan, and Huffman published data on the spectral radiant intensity of thermally excited nitrogen dioxide, NO_2 .^{1*} The measurements, which covered the wavelength region from 460 to 860 nm and the temperature region from 972 to 1335°K, were useful in problems concerned with radiative transport in hot air. Since the measurements are more detailed in wavelength and temperature than published high temperature absorption coefficients,² there is a natural tendency to use the emission intensities^{1,3} to calculate absorption coefficients. When this is done, however, the calculated absorption coefficients show a marked deviation from the measured absorption coefficients²⁻¹¹ as shown in Figure 1. The higher temperature measurements are obtained in part from shock tube data at a few isolated wavelengths and are estimated to have experimental uncertainties on the order of 10 percent.

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*Because of the large number of references mentioned in the above text, please refer to Reference Page No. 23 for References 1 through 11.

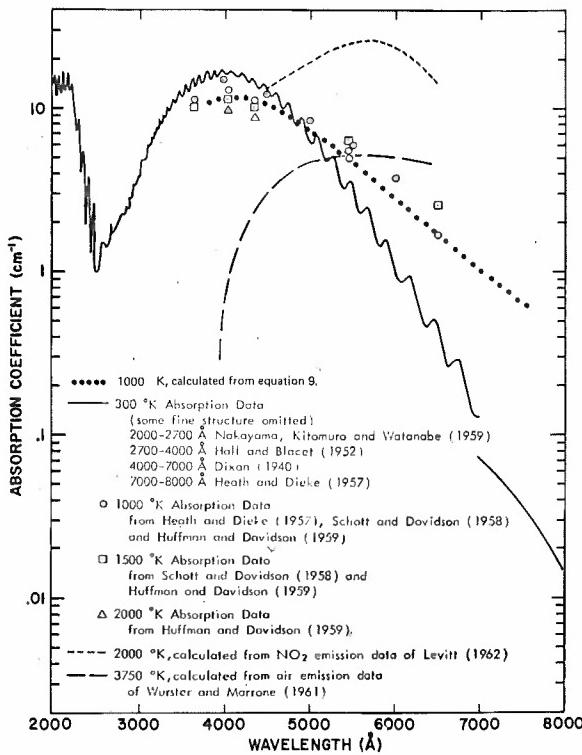


Figure 1. Absorption Coefficients for NO₂ at Various Temperatures and Wavelengths (From Reference 2, in part)

These absorption coefficients at elevated temperatures are of interest because of the importance of NO₂ as an emitter in high-temperature air.² One situation occurs in the lower temperature ranges of the fireball created by atmospheric nuclear detonations. The computer codes used to predict the air opacity and other properties of the highly perturbed atmospheric region resulting from the nuclear detonation require absorption coefficients, or cross-sections, for the absorption of photons by NO₂ and the other constituents of the fireball.

We have obtained NO₂ absorption coefficients in conjunction with our earlier study¹ of emission from hot NO₂. Although the temperature range is not as high as desirable for some uses, the measurements have proved to be of interest to others in connection with fireball models. We are therefore making these absorption coefficients more readily available by the publication of this report.

2. EXPERIMENTAL

Much of the equipment used for these measurements is described in detail in the earlier paper.¹ The major change was the design of the cell. Figure 2 shows the experimental arrangement. The quartz absorption cell was heated with an

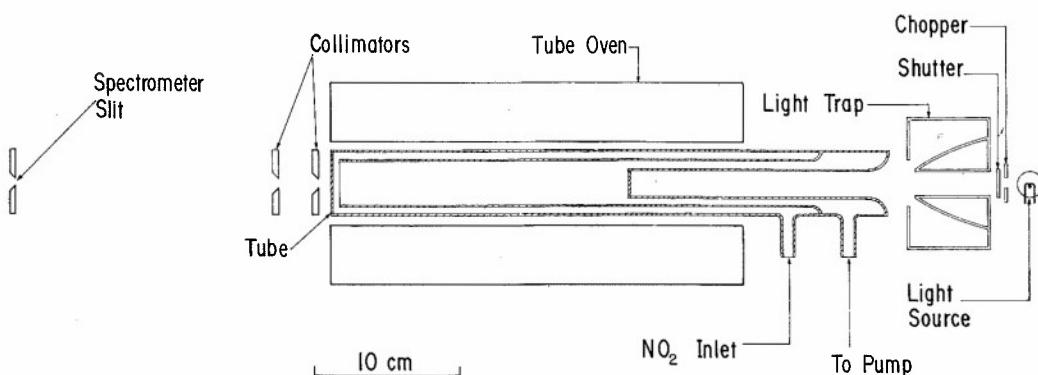


Figure 2. Schematic of High Temperature Absorption Apparatus. The collimators are of cylindrical geometry and are placed so that radiation from the side walls of the cell cannot enter the spectrometer. The entire system was covered to eliminate ambient radiation. Absorption tube was made of quartz

electric tube oven. The cell was designed so that both windows were well within the oven to minimize thermal gradients along the absorption path length. Gas pressures were measured outside the oven with a Pace KP-15 pressure transducer which was calibrated against a mercury manometer. Temperatures were measured with a chromel-alumel thermocouple in good thermal contact with the outside of the cell. A tungsten filament, powered by a current-regulated supply, was used for the light source. The source radiation, which was chopped at 400 Hz with an American Time Products tuning fork chopper, passed through the light trap, the absorption cell, and a series of collimating baffles into the entrance slit of a Spex 3/4 m Czerny-Turner spectrometer, Model 1600. Measurements were made with both slits at 200 μm , which corresponds to a calculated bandwidth of 0.22 nanometers. An EMI 9558 photomultiplier tube was used as the sensor. The photocurrent was amplified by a PAR lock-in amplifier, Model HR-8, and recorded.

Nitrogen dioxide, NO_2 , purified by repeated freezing and pumping until no trace of color (blue-green) could be observed in the white solid, was admitted to the heated cell until the desired pressure was reached. The NO_2 supply was then shut off. Approximately 2 min were necessary to achieve a steady state, as evidenced by variation in the photocurrent due to absorption by the NO_2 . After equilibration, a spectral scan of several tens of nanometers was recorded along with the pressure and the thermocouple readings. Each absorption scan was bracketed by similar scans with the cell evacuated to provide the reference photocurrents. In this manner absorption measurements were made at wavelengths from 380 to 760 nm and at temperatures from 669 to 1313 °K.

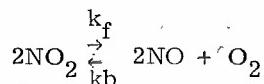
3. RESULTS

The first step in reducing the data is to determine the pressure of NO_2 in the oven. Assuming that the gas in the oven was at thermodynamic equilibrium, the mole fraction of NO_2 was calculated from the equilibrium constant for the dissociation of NO_2 into NO and O_2 , which is obtained from thermodynamic quantities listed in the JANAF Thermochemical Tables.¹² The $2 \text{NO}_2 \rightleftharpoons \text{N}_2\text{O}_4$ equilibrium is not significant at these temperatures. Absorption coefficients at 10-nm intervals are then calculated using the relation

$$k = \frac{760 T}{(273) P \ell} \ln \frac{I_o}{I} \quad (1)$$

where k is in units of cm^{-1} , T is in $^{\circ}\text{K}$, P is the calculated NO_2 pressure, and ℓ is the cell length (20.0 cm).

Preliminary results indicated that k had a significant pressure dependence. Absorption coefficients at high system pressures, near 760 torr, were reasonably constant, but as the system pressure was lowered below about 300 torr an increase in the absorption coefficient was observed. The effect is attributed to the fact that the closed system is partly at oven temperature and partly at room temperature. The dissociation equilibrium



is shifted far to the right at oven temperatures and far to the left at room temperature, thus creating a situation where the NO_2 outside of the oven tends to diffuse into the oven while the NO and O_2 inside the oven tend to diffuse out.

To aid in understanding this effect, data were taken at selected wavelengths and temperatures over a large range in pressures. A typical set of data is shown in Figure 3, where $\log k$, as calculated by Eq. (1), is plotted against $\log P_{\text{System}}$ with $T = 896^{\circ}\text{K}$ and $\lambda = 600 \text{ nm}$. In making these measurements it was obvious that a steady state was attained within a few minutes. Therefore, we write the steady state approximation for the pressure of NO_2 in the oven

$$\frac{d(P_{\text{NO}_2})}{dt} = 0 \approx -k_f (P_{\text{NO}_2})^2 + k_b (P_{\text{NO}})_o^2 (P_{\text{O}_2})_o + D (P_{\text{NO}_2})_a \quad (2)$$

12. JANAF Thermochemical Tables, (1965) Dow Chemical, Midland, Michigan.

where subscript o indicates oven and subscript a indicates ambient temperature, and the last term is the perturbation of equilibrium by diffusion of NO_2 into the oven. Because of their large partial pressures, diffusion of NO and O_2 out of the oven will be less significant.

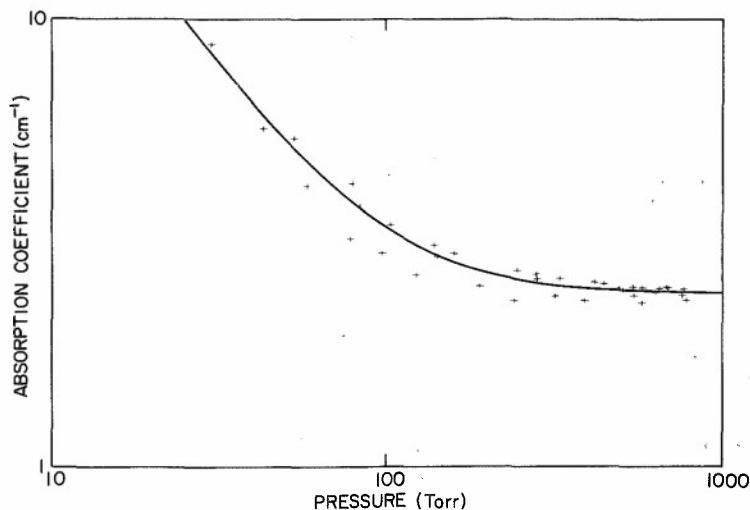


Figure 3. Apparent Absorption Coefficients at 600 Nanometers and 896°K as a Function of System Pressure. The variation in absorption coefficient appears to be due to diffusion of cold NO_2 into the absorption cell as explained in the text. The curve represents a linear regression fit of Eq. (7), the coefficients are shown in Table 1

Equation (2) may be rearranged as

$$(P_{\text{NO}_2})_o = \left[\frac{k_b (P_{\text{NO}})_o^2 (P_{\text{O}_2})_o}{k_f} \right]^{1/2} \left[\frac{D(P_{\text{NO}_2})_a}{1 + \frac{k_b (P_{\text{NO}})_o^2}{k_f} (P_{\text{O}_2})_o} (P_{\text{O}_2})_o \right]^{1/2}. \quad (3)$$

Although the small partial pressure of NO_2 in the oven may change drastically, the percentage effect on NO and O_2 is considerably less. Therefore, it is assumed that the second factor is a perturbation on the equilibrium and that Eq. (3) can be approximated by

$$\begin{aligned} (P_{NO_2}) &= (P'_{NO_2})_o \left\{ 1 + \frac{D(P_{NO_2})_a}{k_b (P_{NO})_o^2 (P_{O_2})_o} \right\}^{1/2} \\ &\approx (P'_{NO_2})_o \left\{ 1 + \frac{2D(1 + \frac{\alpha}{2})^3}{k_b \alpha^3 P_t^2} \right\}^{1/2}. \end{aligned} \quad (4)$$

Ignoring the relatively minor variation of the $(1 + \frac{\alpha}{2})$ factor gives

$$(P_{NO_2})_o \approx (P'_{NO_2})_o \left\{ 1 + \frac{\beta}{\alpha^3 P_t^2} \right\}^{1/2} \quad (5)$$

where $(P'_{NO_2})_o$ is the calculated pressure in the absence of the diffusive perturbation, and α^2 is the fractional dissociation of NO_2 . Equation (1) is rewritten

$$k_{app} = \frac{760}{273} \frac{T}{(P'_{NO_2})_o l} \ln \frac{I_o}{I}$$

where k_{app} is the apparent absorption coefficient based on $(P'_{NO_2})_o$.

It follows that

$$k_{app} (P'_{NO_2})_o = k (P_{NO_2})_o$$

and

$$k_{app} \sim k \left\{ 1 + \frac{\beta}{\alpha^3 P_t^2} \right\}^{1/2} \quad (6)$$

where k is the actual absorption coefficient. The data in Figure 3 were fitted to the relation

$$k_{app}^2 = k^2 + \frac{\beta k^2}{\alpha^3 P_t^2} \quad (7)$$

by linear regression. The quality of the fit is shown by the smooth line in Figure 3. Equation (7) was fitted to sets of data obtained at the temperatures and wavelengths shown in Table 1. The results are tabulated in Table 1 and shown in Figure 4.

For interpolation purposes $\ln \beta$ values were fitted to a quartic in $10^3/T$, which is shown by the smooth curve in Figure 4 and given by

$$\begin{aligned}\ln \beta = & -16.168528 + 24.218754(10^3/T) \\ & -11.448829(10^3/T)^2 - 2.050242(10^3/T)^3 \\ & + 1.281069(10^3/T)^4.\end{aligned}$$

This interpolation formula gives excellent results over the range of experimental data and appears to give reasonable values for minor extrapolations. The variation of β with T is not explained here. However, as derived above, β is proportional to a diffusion coefficient and inversely proportional to a reaction rate constant. It is possible that the perturbing effect of diffusion is overcome at higher temperatures by faster reactions.

Table 1. Coefficients of Eq. (7) for Various Temperatures and Wavelengths

$T(^{\circ}\text{K})$	$\lambda(\text{nm})$	$\beta(\text{atm}^{-2})$	$k(\text{cm}^{-1})$
669	640	2.47×10^{-3}	0.967
763	600	7.29×10^{-3}	1.95
828	600	1.08×10^{-2}	2.23
893	600	1.41×10^{-2}	2.44
980	420	1.58×10^{-2}	11.41
1083	600	1.39×10^{-2}	3.10
1206	500	1.10×10^{-2}	7.54
1315	420	7.82×10^{-3}	11.25

The true absorption coefficient, k , is obtained from

$$k = \frac{760 T}{273 (P'_{\text{NO}_2}) \ell (1 + \beta/\alpha^3 P_t^2)^{1/2}} \ln \frac{I_0}{I}. \quad (8)$$

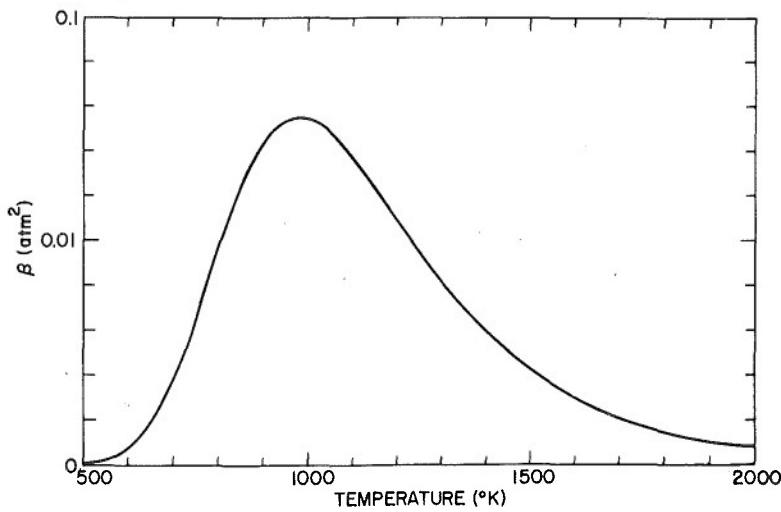


Figure 4. Variation of the Coefficient β of Eq. (7) With Temperature. The curve represents the equation in the text

To illustrate the effectiveness of this correction for diffusion, absorption coefficients were calculated by Eq. (8) for the data which is summarized in Table 1. In order to show the results in a single plot (Figure 5) the data is presented as the percent deviation of k calculated from Eq. (8) and the corresponding value of k , the square root of the intercept of Eq. (7). For the data in Table 1, 20 to 40 different pressures were utilized. The data points are clustered quite tightly at the higher pressures and show more scatter, as would be expected, at lower pressures. The standard deviation of the data shown in Figure 5 is 5.1 percent.

Equation (8) is then used to calculate the absorption coefficients from the larger block of data taken at 10-nm intervals from the absorption scans. The data were obtained at eight temperatures ranging from 669 to 1313°K and over wavelengths ranging from 380 to 760 nanometers. Absorption scans were made at two distinct pressures at each temperature. This resulted in two absorption coefficients at each temperature and selected wavelengths in the regions without overlap, and four absorption coefficients at each temperature and wavelength where there was overlap. In one case, 1317°K and 720 to 760 nm, there was only one absorption scan. To simplify presentation of the data, Tables 2a and 2b list, at each temperature and wavelength, the mean absorption coefficient, the standard deviation, and the number of data points. The data are also shown in Figures 6 through 13, where each measured absorption coefficient is plotted as a function of wavelength for a specific temperature. The smooth curves in the figures are given by the equation

$$k = k_{\max} \exp \left[-1481.3(\Delta E)^2/T \right] \text{ cm}^{-1} \quad (9)$$

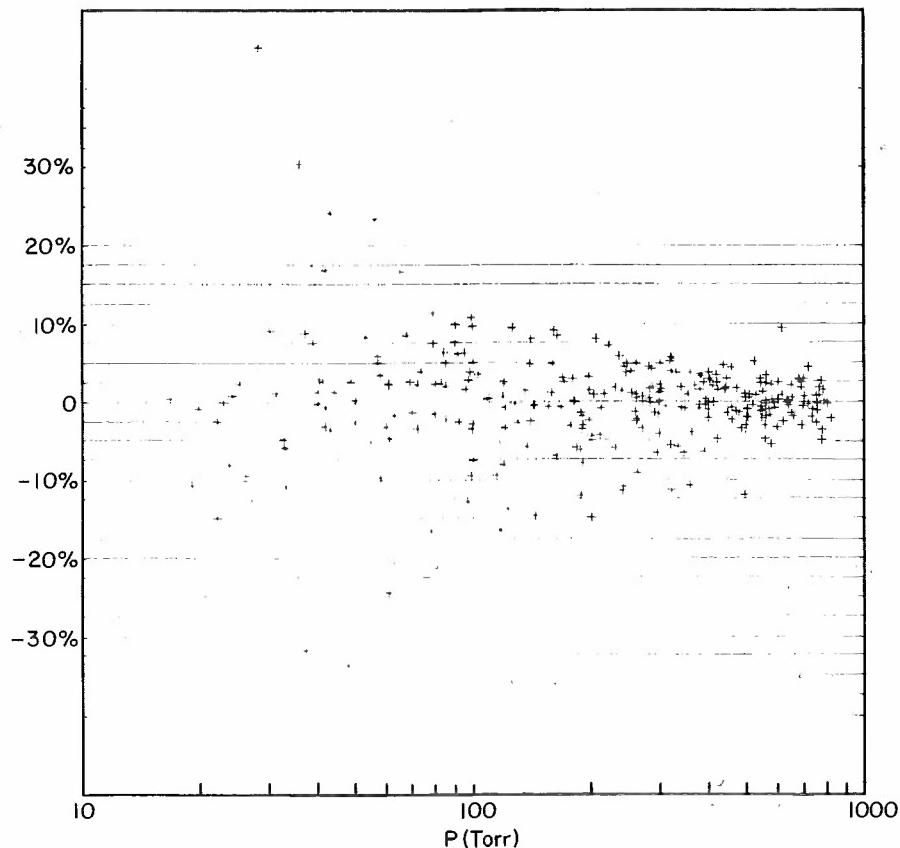


Figure 5. Scatter of Absorption Coefficient Data as a Function of System Pressure. Table 1 data only

where k_{\max} = absorption coefficient at λ_{\max}

$$= \left[\frac{14.84 + 214.3 \exp(-3267/T)}{Q_v} \right] \text{ cm}^{-1}$$

$$\Delta E = \left[E_{\max} - E_{\lambda} \right] \text{ eV}$$

$$E_{\max} = E_{\lambda} \text{ at } \lambda_{\max}$$

$$= 3.04 \text{ eV}$$

$$E_{\lambda} = \left[1239.85/\lambda \right] \text{ eV} \quad (\lambda \text{ in nm})$$

and

Q_v = vibrational partition function for NO_2

$$= \prod_{i=1}^3 (1 - \exp(-h\nu_i/kT))^{-1}.$$

The fundamental mode frequencies listed in Reference 12 are used to evaluate Q_v .

Equation (9) was obtained by linear regression techniques in an effort to understand the thermal variation of the NO_2 absorption coefficient. While the fit to the data is quite good (the linear correlation factor is -0.996 and the F ratio is 101000), this expression is not assumed to have particular theoretical significance. In particular, there is no reason to assume that Eq. (9) can be used for extrapolation to higher temperatures or to wavelengths outside the wavelength range of these measurements.

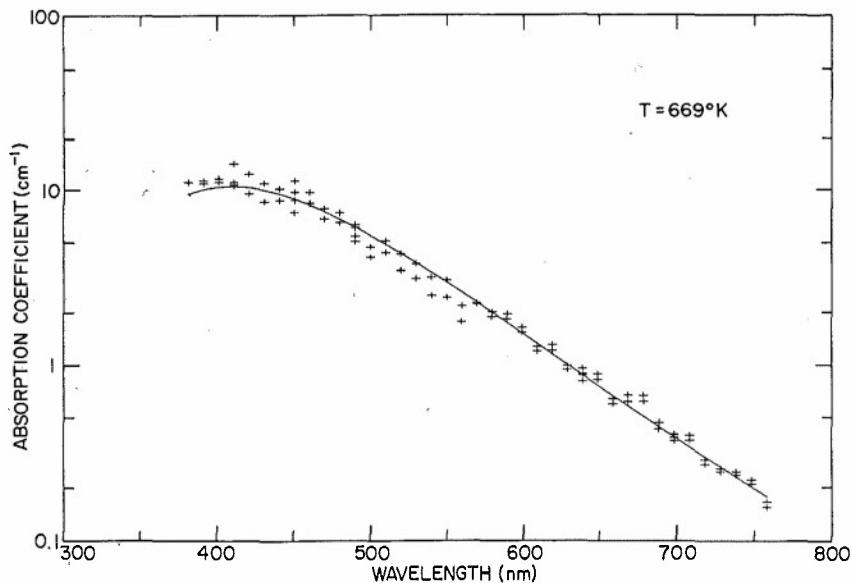


Figure 6. Absorption Coefficient of NO_2 as a Function of Wavelength at 669°K

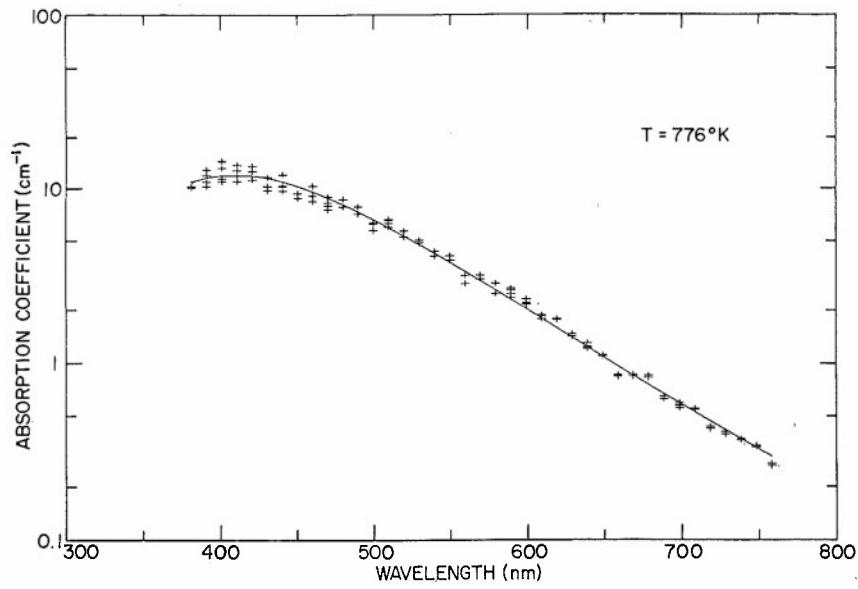


Figure 7. Absorption Coefficient of NO_2 as a Function of Wavelength at 776°K

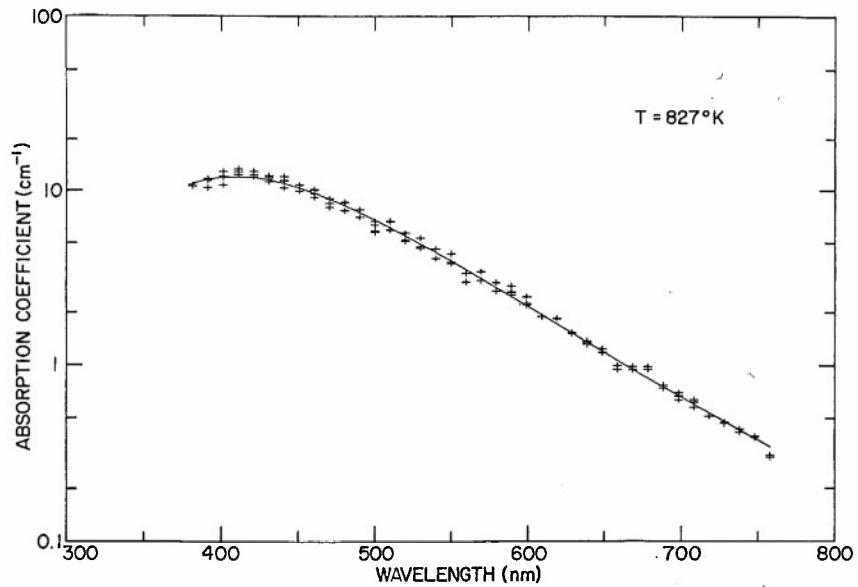


Figure 8. Absorption Coefficient of NO_2 as a Function of Wavelength at 827°K

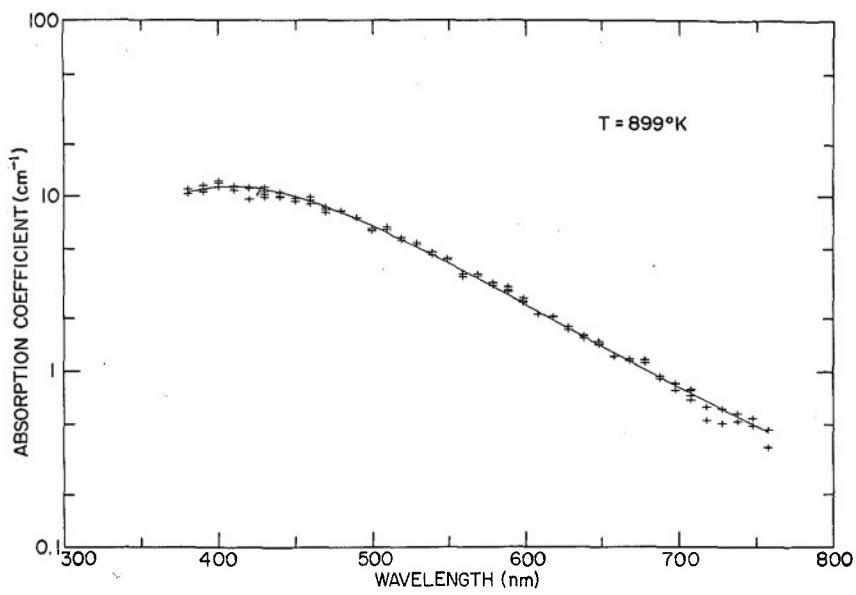


Figure 9. Absorption Coefficient of NO_2 as a Function of Wavelength at 899°K

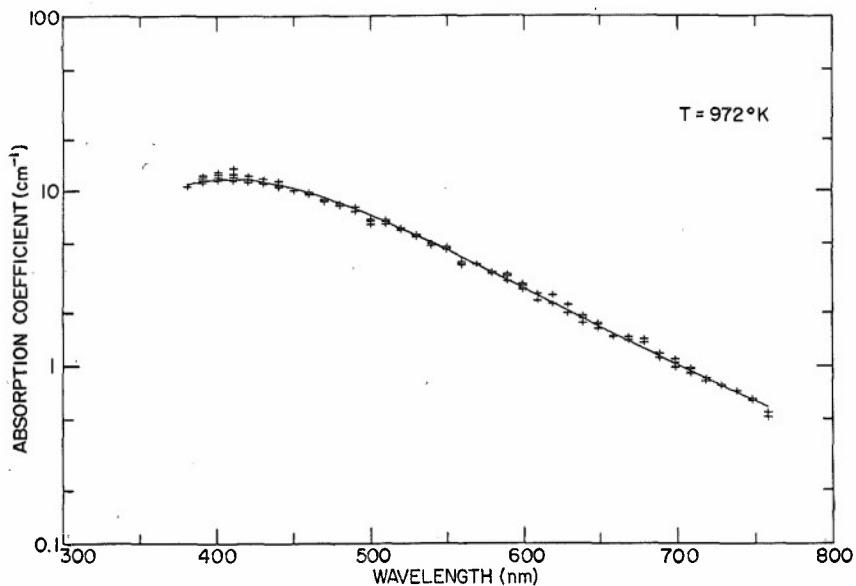


Figure 10. Absorption Coefficient of NO_2 as a Function of Wavelength at 972°K

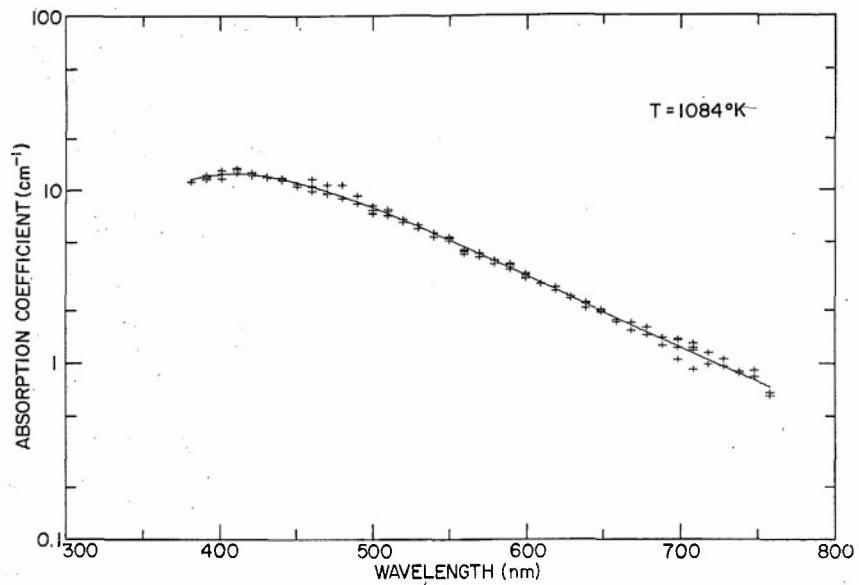


Figure 11. Absorption Coefficient of NO_2 as a Function of Wavelength at 1084°K

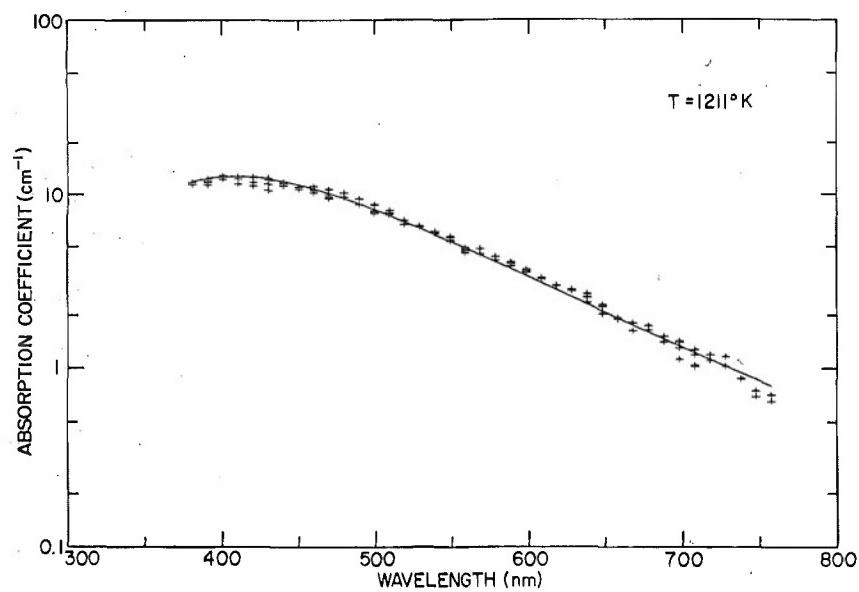


Figure 12. Absorption Coefficient of NO_2 as a Function of Wavelength at 1211°K

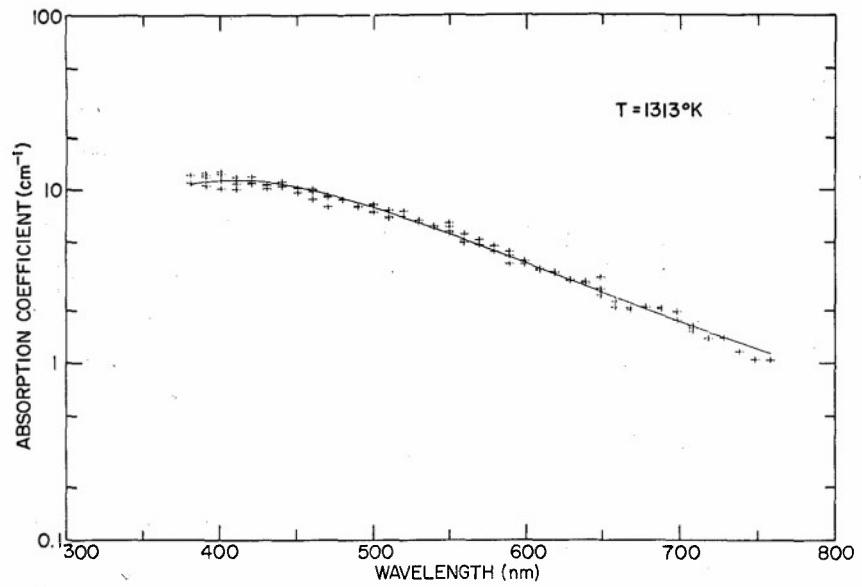


Figure 13. Absorption Coefficient of NO_2 as a Function of Wavelength at 1313°K

Table 2a. Mean Absorption Coefficients, Standard Deviations and Number of Data Points as a Function of Temperature and Wavelength ($\bar{T} = 669 - 899^{\circ}\text{K}$)

Wavelength (nm)	$\bar{T} = 669^{\circ}\text{K}$			$\bar{T} = 776^{\circ}\text{K}$			$\bar{T} = 827^{\circ}\text{K}$			$\bar{T} = 899^{\circ}\text{K}$		
	\bar{k}	s_k	n									
380	11.95	0.01	2	10.54	.12	2	10.87	.16	2	11.08	.49	2
390	11.97	0.33	2	11.90	1.19	4	11.50	.64	4	11.46	.44	4
400	12.26	0.45	2	12.90	1.64	4	12.15	.89	4	12.18	.46	4
410	12.57	1.89	4	12.77	1.19	4	12.96	.47	4	11.68	.29	4
420	11.82	2.18	2	12.91	.95	4	12.59	.43	4	11.20	.80	4
430	10.54	1.83	2	10.85	.83	4	12.04	.41	4	10.99	.61	4
440	10.19	1.12	2	10.96	1.04	4	11.59	.73	4	10.66	.33	4
450	10.04	1.77	2	9.43	.42	2	10.61	.59	2	9.99	.28	2
460	9.75	0.99	2	9.58	.82	4	10.00	.47	4	9.91	.36	4
470	7.91	0.76	2	8.50	.62	4	8.84	.48	4	8.83	.29	4
480	7.51	0.66	2	8.56	.62	2	8.33	.65	2	8.61	.01	2
490	6.17	0.65	4	7.77	.52	2	7.62	.53	2	7.87	.02	2
500	4.74	0.45	2	6.36	.30	4	6.26	.41	5	6.70	.12	4
510	5.09	0.57	2	6.62	.32	4	6.42	.40	5	6.84	.17	2
520	4.15	0.64	2	5.66	.33	2	5.48	.34	3	5.93	.15	2
530	3.67	0.52	2	5.11	.13	2	5.05	.38	3	5.53	.11	2
540	3.00	0.52	2	4.34	.19	2	4.35	.33	3	4.85	.14	2
550	2.89	.48	2	4.09	.17	2	4.10	.30	3	4.52	.06	2
560	2.16	.23	4	3.07	.24	2	3.17	.22	3	3.61	.09	2
570	2.45	.17	2	3.17	.12	2	3.29	.27	2	3.62	.07	2
580	2.03	.10	2	2.72	.27	2	2.86	.23	2	3.20	.09	2
590	1.97	.10	2	2.57	.14	4	2.68	.14	4	2.97	.09	4
600	1.65	.08	2	2.25	.08	4	2.32	.12	4	2.57	.08	4
610	1.28	.06	2	1.85	.05	4	1.92	.00	2	2.14	.00	2
620	1.30	.07	2	1.80	.02	2	1.87	.02	2	2.08	.00	2
630	1.00	.04	2	1.45	.03	2	1.54	.02	2	1.78	.05	2
640	.912	.064	4	1.25	.04	4	1.36	.03	4	1.58	.03	4
650	.885	.049	2	1.11	.01	2	1.21	.03	4	1.45	.03	4
660	.640	.030	2	.849	.015	2	.980	.034	2	1.22	.00	2
670	.664	.041	2	.852	.015	2	.970	.028	2	1.16	.02	2
680	.664	.037	2	.840	.017	2	.971	.024	2	1.14	.03	2
690	.462	.028	2	.634	.017	2	.759	.019	2	.923	.023	2
700	.401	.016	4	.573	.017	4	.667	.026	4	.830	.037	4
710	.395	.018	2	.544	.005	2	.612	.026	4	.741	.047	4
720	.288	.012	2	.427	.008	2	.511	.001	2	.570	.070	2
730	.258	.007	2	.396	.010	2	.469	.006	2	.554	.076	2
740	.248	.008	2	.363	.004	2	.423	.013	2	.541	.041	2
750	.222	.008	2	.332	.004	2	.388	.004	2	.511	.035	2
760	.165	.008	2	.260	.006	2	.303	.006	2	.411	.068	2

Table 2b. Mean Absorption Coefficients, Standard Deviations and Number of Data Points as a Function of Temperature and Wavelength ($\bar{T} = 972 - 1313^{\circ}\text{K}$)

Wavelength (nm)	$\bar{T} = 972^{\circ}\text{K}$			$\bar{T} = 1084^{\circ}\text{K}$			$\bar{T} = 1211^{\circ}\text{K}$			$\bar{T} = 1313^{\circ}\text{K}$		
	\bar{k}	s_k	n	\bar{k}	s_k	n	\bar{k}	s_k	n	\bar{k}	s_k	n
380	10.94	.00	2	11.38	.00	2	11.80	.22	2	11.94	.90	2
390	12.12	.51	4	12.07	.32	4	11.99	.39	4	12.13	.87	4
400	12.58	.62	4	12.59	.57	4	12.72	.25	4	12.03	1.19	4
410	12.84	.91	4	13.26	.40	4	12.51	.56	4	11.38	.78	4
420	12.03	.49	4	12.70	.28	4	12.24	.67	4	11.55	.49	4
430	11.68	.37	4	12.15	.13	4	11.89	.84	4	10.91	.29	4
440	11.28	.42	4	11.83	.18	4	11.74	.28	4	11.03	.32	4
450	10.44	.04	2	10.91	.27	2	11.13	.21	2	10.29	.44	2
460	10.05	.14	4	10.82	.74	4	10.88	.38	4	10.02	.60	4
470	9.09	.12	4	10.07	.59	4	10.19	.54	4	9.20	.64	4
480	8.64	.20	2	10.05	1.25	2	10.15	.40	2	9.11	.02	2
490	8.13	.31	2	8.99	.67	2	9.29	.49	2	8.27	.07	2
500	6.93	.20	4	7.72	.39	4	8.29	.44	4	8.08	.46	4
510	6.88	.16	4	7.48	.28	4	7.96	.21	4	7.49	.43	4
520	6.25	.12	2	6.76	.21	2	7.04	.28	2	7.52	.40	2
530	5.69	.11	2	6.20	.20	2	6.65	.03	2	6.78	.17	2
540	5.07	.10	2	5.59	.24	2	6.15	.10	2	6.30	.09	2
550	4.81	.07	4	5.30	.11	5	5.64	.16	4	6.14	.38	4
560	3.92	.07	4	4.44	.10	5	4.84	.14	4	5.28	.28	4
570	3.90	.00	2	4.27	.13	3	4.76	.25	2	5.10	.25	2
580	3.47	.06	2	3.89	.11	3	4.32	.16	2	4.66	.25	2
590	3.29	.12	4	3.65	.11	5	4.03	.09	4	4.19	.29	4
600	2.87	.10	4	3.21	.10	5	3.63	.06	4	3.90	.08	4
610	2.52	.16	2	2.88	.01	2	3.29	.04	2	3.53	.05	2
620	2.44	.21	2	2.68	.08	2	2.99	.00	2	3.38	.04	2
630	2.14	.17	2	2.40	.04	2	2.81	.03	2	3.04	.04	2
640	1.89	.09	4	2.18	.08	4	2.55	.12	4	2.93	.05	4
650	1.73	.06	4	1.99	.04	4	2.23	.12	4	2.75	.30	4
660	1.47	.00	2	1.73	.03	2	1.93	.03	2	2.21	.12	2
670	1.44	.04	2	1.61	.13	2	1.73	.13	2	2.08	.04	2
680	1.40	.05	2	1.52	.11	2	1.71	.07	2	2.12	.01	2
690	1.15	.05	2	1.32	.10	2	1.47	.07	2	2.08	.03	2
700	1.03	.06	4	1.24	.15	4	1.32	.14	4	1.85	.13	3
710	.938	.033	4	1.15	.17	4	1.13	.12	4	1.59	.06	3
720	.834	.023	2	1.05	.11	2	1.15	.06	2	1.39	—	1
730	.773	.006	2	.995	.070	2	1.10	.10	2	1.41	—	1
740	.714	.003	2	.875	.016	2	.871	.004	2	1.17	—	1
750	.637	.011	2	.859	.054	2	.713	.036	2	1.05	—	1
760	.524	.023	2	.654	.021	2	.674	.040	2	1.04	—	1

4. DISCUSSION

The precision of the measurements is about 5 percent, which is the typical standard deviation of the absorption coefficient at a given wavelength and temperature. It is difficult to assess the accuracy of these measurements. Total pressure is known to better than 2 percent. Photocurrents are typically measured to about 1 percent accuracy. The temperatures are measured to $\pm 3^{\circ}\text{K}$.

The determination of the pressure of NO_2 in the absorption cell is the main source of inaccuracy. The thermochemical data¹² should be quite accurate. The calculated NO_2 pressure, under isothermal conditions, would probably be accurate to ± 2 or 3 percent. However, part of the system is at low temperatures and this introduces the perturbation to equilibrium which is described in the previous section. We believe that the empirical approach to this problem has reduced the inaccuracy of the cross-sections to ± 10 percent. A comparison of our data to the previously published absorption coefficients (see Figure 1) shows that the present results lie close to or a little below the previously published data. The discrepancies lie within the experimental uncertainties of the measurements.

These results therefore support the previous data and provide more detailed information. They do not provide absorption coefficients for NO_2 at temperatures beyond about 1500°K .

At higher temperatures, it is not recommended that emission intensities from shock tube³ or other experiments¹ be converted into the corresponding absorption coefficients for NO_2 . As shown in Figure 1, absorption coefficients which are calculated from shock tube emission intensities are considerably different from the measured absorption coefficients for NO_2 . We have also calculated the absorption coefficients from the emission intensities obtained with the same equipment;¹ the results were similar to those shown by Gilmore.²

These results are considered to be only an apparent contradiction of Kirchoff's Law. It has been known for some time^{13, 14} that the radiative transitions of NO_2 exhibit "anomalous" behavior. For example, the fluorescent radiative lifetimes for NO_2 are much longer than that which is calculated from the integrated absorption coefficient. The molecule is a relatively complex system, with a bent ground state and several linear and bent excited states 2 to 3 eV above the ground state. The exact configurations of these excited states are largely unknown. Due to the variety of possible interactions, perturbations, radiationless transitions, etc., that can take place it is not surprising that anomalous results are observed.

13. Neuberger, D. and Duncan, A.E.F. (1954) J. Chem. Phys. 22:1963.

14. Douglas, A.E. (1966) J. Chem. Phys. 45:1007.

The system is complicated enough so that the related emission and absorption processes cannot be isolated in the observed spectra, and therefore an application of Kirchoff's Law appears to be not readily possible. The separate measurement in the same laboratory of the thermal emission¹ and the absorption coefficient reported here should amply demonstrate this situation. Therefore, it is recommended that computer codes not convert emission data to absorption data and vice-versa for the NO₂ molecule, since the present results, coupled with earlier measurements, demonstrate errors in this technique. If absorption coefficients are required, only measured values should be used.

References

1. Paulsen, D. E., Sheridan, W. F., and Huffman, R. E. (1970) J. Chem. Phys. 53:647.
2. Gilmore, F. R. (1965) J. Quant. Spectry. Radiative Transfer 5:125 and references therein.
3. Levitt, B. P. (1965) J. Chem. Phys. 42:1038.
4. Dixon, J. K. (1940) J. Chem. Phys. 8:157.
5. Hall, T. C. and Blacet, F. E. (1952) J. Chem. Phys. 20:1745.
6. Heath, D. F. and Dieke, G. H. (1957) Absorption of NO₂, unpublished, included in Reference 2.
7. Schott, G. and Davidson, N. (1958) J. Am. Chem. Soc. 80:1841.
8. Huffman, R. E. and Davidson, N. (1959) J. Am. Chem. Soc. 81:2311.
9. Nakayama, T., Kitamura, M., and Watanabe, K. (1959) J. Chem. Phys. 30:1180.
10. Wurster, W. H. and Marrone, P. V. (1961) Study of Infrared Emission in Heated Air, QM-1373-A-4, Cornell Aeronautical Laboratory, Buffalo, New York.
11. Levitt, B. P. (1962) Trans. Faraday Soc. 58:1789.
12. JANAF Thermochemical Tables, (1965) Dow Chemical, Midland, Michigan.
13. Neuberger, D. and Duncan, A. E. F. (1954) J. Chem. Phys. 22:1963.
14. Douglas, A. E. (1966) J. Chem. Phys. 45:1007.

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